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3 **Scattering Calculations for Asymmetric Rain Drops**

4 **during a Line Convection Event: Comparison with Radar**

5 **Measurements**

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ABSTRACT

Two-dimensional video disdrometer (2DVD) data from a line convection rain event are analyzed using the method of moments surface integral equation (MoM-SIE) via drop-by-drop polarimetric scattering calculations at C-band which are compared with radar measurements. Drop geometry of asymmetric drop shapes is reconstructed from 2DVD measurements and the MoM-SIE model is created by meshing the surface of the drop. The Z_{dr} calculations for an example asymmetric drop are validated against an industry standard code solution at C-band, and azimuthal dependence of results is documented. Using the MoM-SIE analysis on 2DVD drop-by-drop data (also referred to as simply MoM-SIE), the radar variables [Z_h , Z_{dr} , K_{dp} , ρ_{hv}] are computed as a function of time (with 1-minute resolution) and compared to C-band radar measurements. The importance of shape variability of asymmetric drops is demonstrated by comparing with the traditional (or, ‘bulk’) method which uses 1-minute averaged drop size distributions and equilibrium oblate shapes. This was especially pronounced for ρ_{hv} where the MoM-SIE method showed lowered values (dip) during the passage of the line convection consistent with radar measurements, unlike the bulk method. The MoM-SIE calculations of [Z_h , Z_{dr} , K_{dp}] agree very well with the radar measurements whereas LDR calculations from drop-by-drop method are found to be larger than the values from the bulk method which is consistent with the dip in simulated as well as radar-measured ρ_{hv} . Our calculations show the importance of the variance of shapes due to asymmetric drops in the calculation of ρ_{hv} and LDR.

40 **1. Introduction**

41 Polarimetric weather radars make use of the oblate shapes and high degree of orientation
42 of raindrops in order to better estimate rainfall rates from the retrieved raindrop size
43 distributions (Seliga and Bringi 1976; 1978). As a first step, they utilize the differential
44 reflectivity (Z_{dr}) along with the conventionally measured co-polar reflectivity (Z_h), to reduce
45 uncertainties in estimating the drop size distribution within the radar pulse volume (Bringi
46 and Chandrasekar 2001).

47 The equilibrium shapes of raindrops are size dependent (Beard and Chuang 1987) and
48 they are generally approximated by oblate spheroids whose axis ratios (minor to major)
49 decrease monotonically with increasing size. Drops with diameters smaller than 0.8 mm can
50 be considered almost spherical. For larger drops (>2.5 mm) the concept of dynamic
51 equilibrium shape was introduced by Szakáll et al. (2009) to describe the time-averaged axis
52 ratios due to drop oscillations observed in a wind tunnel which was also confirmed using the
53 concept of ‘most probable’ shapes from 2-D video disdrometer (2DVD; Schönhuber et al.
54 2008) by Thurai et al. (2009a). It is now well-known that axisymmetric drop oscillations
55 dominate the background state with smaller amplitude mixed oscillation modes that give rise
56 to *asymmetric* shapes (Beard et al. 2010). However, there is no theoretical framework for
57 modeling such *asymmetric* shapes in natural rainfall. Hence, the common approach is to
58 neglect the variance of drop shapes and to relate the mean axis ratio with drop equi-volume
59 diameter (D_{eq}) (Beard and Chuang 1987; Brandes et al. 2004; Thurai et al. 2007).

60 *Asymmetric* drops were inferred from 2DVD measurements in a highly-organized line
61 convection rain event described in Thurai et al. (2013). During this event a significant
62 fraction of drops (around 30%) within the line convection were *asymmetric*. Eight individual
63 *asymmetric* drops were chosen from the 2DVD measurements to reconstruct their 3D-shapes

64 (Thurai et al. 2017) and to determine their individual scattering amplitudes at C-band using
65 the method of moments in the surface integral formulation (MoM-SIE) (Chobanyan et al.
66 2015). Scattering calculations for the individual asymmetric drops showed that the single
67 particle differential reflectivity (Z_{dr}) values differed from those calculated assuming
68 rotationally symmetric shapes. Differences were also seen in the case of (single particle)
69 specific differential phase (K_{dp} factor) as well as linear depolarization ratio (LDR).

70 Accurate simulations of radar observables require accounting for variance of drop shapes
71 which requires computation of drop-by-drop scattering amplitudes and integration of the
72 elements of the covariance matrix over a given measurement interval (Bringi and
73 Chandrasekar 2001). The aforementioned line convection event is analyzed in this manner
74 herein using 3D- reconstruction of drop shapes from 2DVD disdrometer data. Radar
75 reflectivity, differential reflectivity, copolar correlation coefficient and specific differential
76 phase are computed with 1-min time resolution and compared to radar measurements
77 extracted over the 2DVD site from the University of Alabama in Huntsville Advanced Radar
78 for Meteorological and Operational Research (ARMOR) C-band radar (see Petersen et al.
79 2007; Crowe et al. 2012). The radar is 15 km away from the ground instrument site and the
80 height of the resolution volume is around 340 m at the lowest elevation angle of 1.3° . For
81 completeness the linear depolarization ratio is also computed even though the radar is not
82 configured for measuring LDR. The drop-by-drop scattering simulations are compared with
83 the bulk method which refers to the use of the T-matrix scattering code (Barber and Yeh
84 1975) with input being the 1-minute averaged drop size distributions from 2DVD, the oblate
85 axis ratios from Thurai et al. (2007) with Gaussian canting angle distribution [mean= 0° ,
86 $\sigma=5^\circ$].

87 This paper is organized as follows. In Section 2, we revisit the methodology used to
88 obtain the scattering results. Section 3 is reserved for the details of raindrop model
89 construction, used as input to the scattering code. In Section 4, for validation purposes, we
90 consider an example of an *asymmetric* drop that is reconstructed from 2DVD measurements
91 (Thurai et al. 2017) and the results obtained by our electromagnetic solver (MoM-SIE) are
92 compared to those using an industry standard software. We then consider, in Section 5, the
93 line convection event and compare radar measurements with scattering simulations using
94 drop-by-drop as well as the bulk method. The paper concludes with a short Discussion and
95 Conclusions section.

96

97 **2. Methodology: numerical solution**

98 Raindrop scattering calculations assuming oblate (or rotationally symmetric) shapes
99 typically use the T-matrix method (Waterman 1965; Barber and Yeh 1975; Mishchenko et al.
100 1996) which is widely used by the radar meteorology community (see, also, Chobanyan et al.
101 2015 and references therein for a review of different scattering methodologies including
102 discrete dipole approximation, surface and volume integral formulations used for
103 precipitation particles).

104 Scattering calculations are performed herein using a higher order method of moments
105 solution to the electric and magnetic field surface integral equations (MoM-SIE) based on
106 boundary conditions between air and water dielectric at the rain drop surface, S_a , i.e., the
107 continuity of tangential components of total (incident plus scattered) electric/magnetic fields
108 (Notaroš 2008; Djordjević and Notaroš 2004)

109 In our current work using the MoM-SIE methodology, a geometrical model is obtained
110 by discretization of the raindrop surface using Lagrange-type curved parametric quadrilateral

111 elements of arbitrary orders (Djordjević and Notaroš 2004; Chobanyan et al. 2015). The
 112 method directly solves for an approximation of fictitious surface electric and magnetic
 113 current densities, \mathbf{J}_s and \mathbf{M}_s , over the rain drop boundary using hierarchical divergence-
 114 conforming polynomial basis functions, defined over quadrilateral elements (Djordjević and
 115 Notaroš 2004; Chobanyan et al. 2015).

116 For a given incident wave, the scattered electric field is represented as the following
 117 function of current densities:

$$118 \quad \mathbf{E}^{\text{scat}}(\mathbf{J}_s, \mathbf{M}_s, \varepsilon) = -j\omega\mu_0 \int_{S_a} (\mathbf{J}_s g + k^{-2} \nabla_s \cdot \mathbf{J}_s \nabla g) dS_a + \int_{S_a} \mathbf{M}_s \times \nabla g dS_a \quad (1)$$

119 where g ($g = e^{-jkR} / 4\pi R$) and k ($k = \omega\sqrt{\varepsilon\mu_0}$), respectively, are Green's function and wave
 120 number for the unbounded medium of parameters $\varepsilon = \varepsilon_r \varepsilon_0$ and μ_0 , with R being the distance
 121 of the field point from the source point, $\omega = 2\pi f$ the angular (radian) frequency, and ε_r the
 122 dielectric constant of the rain drop (water). Magnetic field is expressed in a similar fashion.

123 When the distance R in (1) is zero or relatively small, the singular or near-singular terms
 124 are extracted and evaluated analytically, and the remaining non-singular integrals are
 125 calculated numerically using Gauss-Legendre integration formulas. The final matrix equation
 126 is obtained after the Galerkin testing procedure has been applied to boundary condition
 127 equations, which assumes another surface integration of the SIEs with testing (weighting)
 128 functions being equal to the basis functions.

129 For verification purposes, another method that utilizes 3-D geometrical discretization is
 130 considered and results are presented in terms of single particle dual-polarization scattering for
 131 three different frequency bands.

132

133 **3. Raindrop modelling**

134 Drop shapes recorded by the 2DVD are used for 3D-reconstruction (for $D_{eq} > 2$ mm)
135 using the algorithm in Schönhuber et al. (2016). Drops with $D_{eq} < 2$ mm are assumed to have
136 oblate spheroidal shapes with axis ratio as a function of D_{eq} given in (Thurai et al. 2007). The
137 3D-reconstruction procedure give rises to more significant errors for small drops (due to
138 resolution of $170 \mu\text{m}$) and hence the 2 mm threshold was applied. Note also that the larger
139 drops will have more of an effect on Z_{dr} than the small drops.

140 Details of the 3D-shape reconstruction of each recorded drop from its images from the
141 two orthogonal cameras have been published previously (Schönhuber et al. 2016; Schwinzerl
142 et al., 2015) hence only a brief summary is given here. The 2DVD measures drop contours in
143 two perpendicular planes which can be skewed due to horizontal component of the drop
144 velocity (typical in line scan camera systems). For drops that possess an axis of symmetry,
145 the contours can be deskewed as described in (Schönhuber et al. 2000; Huang et al. 2008); in
146 addition, the horizontal velocity can be estimated. In the Appendix of Thurai et al. (2017), the
147 horizontal drop velocities derived from the deskewing procedure were shown to be in
148 excellent agreement with the independent wind sensor measurements, both in magnitude and
149 in direction. For deskewing *asymmetric* drops the horizontal velocity must be estimated. This
150 is achieved from the drop horizontal velocities estimated from the deskewed symmetric drops
151 closest in time and size to the *asymmetric* drop (see Section IV of Schönhuber et al., 2016).
152 One limitation of this method for *asymmetric* drops relates to the uncertainty in the exact
153 drop horizontal velocity required as input to the deskewing procedure. However, apart from
154 errors due to rapid fluctuations in wind velocities, we expect the reconstructed shapes to be
155 reasonably representative of their true ‘instantaneous’ shapes.

156 The deskewed contours in the two orthogonal planes are sampled at equidistant values
157 along the vertical axis and four points are obtained at each height (note that for rotationally

158 symmetric drops the thin ‘slices’ along the vertical axis are elliptical and the 3D shape is
159 based on stacked ellipses). For asymmetric drops, four different ellipse quarters are
160 constructed for each slice having in mind the center point. The points describing the
161 geometry of each slice are obtained by sampling the constructed elliptical quarters in uniform
162 intervals of the azimuth angle. The procedure is repeated for each slice in order to create the
163 3D-reconstructed drop, an example of which is shown in Fig. 1. In our models, the shapes of
164 the slices are limited to convex shapes, i.e. the center point needs to be inside or part of the
165 circumference.

166 The model of the drop is created by defining first order (bilinear) quadrilateral elements,
167 each between four points of the geometry (Thurai et al. 2017). To define one element, two
168 points are chosen with the same coordinate value on the z axis and sequential values on the
169 azimuthal coordinate. Two other points are chosen to have the same azimuth angles but
170 different, consecutive z axis values compared to the two already chosen points. After creating
171 all the elements by connecting pairs of points from groups with consecutive values on the z
172 axis, the elements at the top and the bottom of the drop are defined using all four points from
173 the group having the same z axis value, the highest and the lowest, respectively, so the entire
174 surface of the drop is discretized. The order of the basis functions (Djordjević and Notaroš
175 2004) used for the unknown expansion over the elements was chosen to comply with Klopff et
176 al. (2012).

177

178 **4. Validation of the MoM-SIE method**

179 The single particle differential reflectivity, Z_{dr} (expressed as a ratio) is given by:

$$Z_{\text{dr}} = \frac{|S_{\text{hh}}|^2}{|S_{\text{vv}}|^2} \quad (2)$$

180 where S_{hh} and S_{vv} are the frequency-dependent backscatter amplitudes for horizontal (h) and
 181 vertical (v) polarizations. Fig. 2 shows the calculated Z_{dr} for the reconstructed drop in Fig. 1
 182 as a function of the (‘look’) azimuthal angle ϕ , for S, C, and X bands. In all three cases, the
 183 Z_{dr} variation with ϕ is significant, whereas for a rotationally symmetric drop the Z_{dr} is ϕ -
 184 independent, with values of 3.0, 3.7, and 3.2 dB, respectively, marked as ‘+’ points. Fig. 2
 185 also shows that C-band variation lies well above the S and X band variations, which can be
 186 attributed to this particular drop size ($D_{\text{eq}} = 4.81$ mm) lying in the C-band resonance
 187 scattering region (e.g., Carey and Petersen, 2015). The ϕ -angle variation at C-band is also
 188 slightly higher than those at S and X bands.

190 Although Fig. 2 shows a somewhat periodic variation with the ϕ -angle for all three
 191 frequency bands, the real and imaginary parts of S_{hh} and S_{vv} do not necessarily show the same
 192 trend. As an example, Fig. 3 shows these variations for C-band. The imaginary part of S_{hh} and
 193 S_{vv} show non-periodic variations but their amplitudes are considerably lower than the
 194 corresponding real parts. It turns out that the Z_{dr} variation is much more governed by the
 195 variation in $Re(S_{\text{hh}})$ and $Re(S_{\text{vv}})$ than by $Im(S_{\text{hh}})$ and $Im(S_{\text{vv}})$.

196 By way of verification of the MoM-SIE based scattering amplitude results, another
 197 method that uses 3-D discretization, namely, ANSYS HFSS code² (industry standard utilizing
 198 the volumetric finite element method – FEM, so numerically very different from the MoM-
 199 SIE approach), is employed. Results by the FEM (HFSS) with the computational region
 200 truncated by means of a perfectly matched layer (PML) are also included in Figs. 3(a) and

² See: <http://www.ansys.com/products/electronics/ansys-hfss>

201 3(b). As can be seen, the resulting scattering amplitudes are very close to the MoM-SIE based
202 results. MoM-SIE methods are computationally efficient for electromagnetic problems with
203 small volume to surface ratio and when Green's function can be calculated³. FEM-based
204 codes are widely used in computational electromagnetics (in industry), but require
205 discretization of the whole 3 dimensional domain as well as region truncation with boundary
206 condition in order to compute far field scattering results that are easily computed by the SIE
207 method.

208

209 **5. Calculation of radar variables and comparisons with radar**

210 **measurements**

211 We now consider the rain event which occurred in Huntsville, Alabama on 25 December
212 2009. This was a wide spread event with an embedded line convection which traversed the
213 disdrometer site (Thurai et al., 2013). The 2DVD measurements for this event showed that a
214 significant fraction of the drops within the line convection (around 30%) did not possess any
215 rotational symmetry axis (i.e., *asymmetric*).

216 Altogether, 2DVD measurements over a period of 100 minutes were analysed during
217 which there were 114,317 drops recorded by the instrument, out of which 10,233 drops had
218 $D_{\text{eq}} \geq 2$ mm. For all the drops with $D_{\text{eq}} \geq 2$ mm, the 3D shapes were constructed in the same
219 way as outlined in Thurai et al. (2017), and their individual scattering amplitudes were
220 calculated using the MoM-SIE method. The individual particle Z_{dr} are plotted as time series
221 in Fig. 4 for two values of incident angle. The top two panels show the Z_{dr} for all drops with
222 $D_{\text{eq}} \geq 2$ mm for the entire 100-minute period whilst the two lower panels show the same but

³ See: https://en.wikipedia.org/wiki/Computational_electromagnetics

223 for the zoomed in time period. In all cases, the drop sizes are color-coded. The variability in
224 Z_{dr} for a given drop size is particularly evident for the large drops (> 4 mm) and further the
225 dependence on the azimuthal angle is also evident. For all drops with $D_{eq} < 2$ mm, oblate
226 shapes were assumed whose axis ratios were determined using the diameter-dependent
227 relationship given in Eq. (2) of Thurai et al. (2007). For these drops, the individual scattering
228 amplitudes were also computed with the MoM-SIE. The variability of the single particle Z_{dr}
229 during the line convection passage is evident from Fig. 4(c) though some of the variability is
230 due to sampling errors for the larger sizes which are much lower in concentration. With this
231 consideration the variability in single particle Z_{dr} for a given D_{eq} reflects the variance in
232 shapes due, in part, to the *asymmetric* drops. The coefficient of variation of Z_{dr} (expressed as
233 a ratio) for sizes > 3 mm is around 0.5. The coefficient of variation of the “effective” axis
234 ratio is then ≈ 0.2 using the approximate formula from Jameson (1983). The deduced axis
235 ratio variability is around twice that found by Thurai et al. (2009a) due to *asymmetric* drops.

236 From the backscatter amplitudes of each individual drop over a finite time period (1-
237 minute) and drop-by-drop integration of the relevant covariance matrix elements (Bringi and
238 Chandrasekar 2001), the radar reflectivity for horizontal polarization (Z_h), differential
239 reflectivity (Z_{dr}) and copolar correlation coefficient (ρ_{hv}) were computed, for comparisons
240 with the C-band ARMOR radar measurements (see Eqs. 3-6, later in the text). This method
241 will also be referred to as the MoM-SIE. Note that for K_{dp} calculation the forward scatter
242 amplitudes are used. The finite time period chosen here is 1-minute, since for smaller
243 averaging period, the sampling errors will be large (Schuur et al. 2001) and for larger
244 averaging period, drop sorting errors will also be large (Lee and Zawadzki 2005). Note from
245 Fig. 4 (c) and (d) that the line convection passage over the disdrometer site took around 15
246 minutes, from 03:33 UTC to 03:48 UTC.

247 Fig. 5 shows the PPI (plan position indicator) scan taken with the ARMOR radar
248 (Petersen et al. 2007) at an elevation angle of 1.3 deg. The time of the scan was 03:40 UTC.
249 The ‘star’ mark represents the location of the 2DVD, and at this time the line convection was
250 directly positioned over the disdrometer site. Panels (a) and (b) show the copolar reflectivity
251 and the differential reflectivity after correcting for attenuation and differential attenuation,
252 respectively. The correction procedures use the specific differential propagation phase based
253 algorithms, using the same procedure described in Bringi et al. (2006). Reflectivity values
254 were high at the site (> 50 dBZ) and differential reflectivity values were also high (> 4 dB)
255 indicating large drops in the strong precipitation shaft. Other PPI scans taken before and after
256 03:40 UTC can be seen from Fig. 7 in Thurai et al. (2013). Panel (c) shows the corresponding
257 copolar correlation coefficient, ρ_{hv} , and panel (d) marks the areas within the line convection
258 where ρ_{hv} was less than 0.9. Values of attenuation-corrected Z_h and Z_{dr} as well as ρ_{hv} were
259 extracted near and around the radar pixels surrounding the 2DVD site (14.5 km radar range,
260 52.7 degree azimuth) from all the PPI sweeps that were taken from 03:00 to 04:40 UTC. For
261 a given elevation angle, each sweep was repeated at 5-minute time interval.

262 The extracted Z_h and Z_{dr} are shown in Figs. 6(a) and 6(b), respectively, for the 100-
263 minute period. For a given PPI sweep time, several points are shown which correspond to the
264 ‘2DVD-pixel’ as well as the ‘immediate adjacent’ pixels in both azimuth and range, covering
265 approximately an area of 750 m by 750 m over the 2DVD site. Altogether 20 PPI sweeps
266 were used over the entire 100-minute period. Reflectivity and differential reflectivity values
267 reach their highest values at 03:40 UTC. Later on, at around 04:30 UTC, reflectivity values
268 again rise but only up to 40 dBZ. Differential reflectivity remains relatively low, indicating
269 that the maximum drop sizes were significantly lower at 04:30 than at 03:40 UTC. The
270 measured drop size distributions (DSDs) can be seen from Fig. 2(b) in Thurai et al. (2013).

271 At 03:40, the spectra showed the highest mass-weighted mean diameter and the highest
 272 standard deviation of the mass spectrum (not shown).

273 Over-plotted in black in Figs. 6(a) and 6(b) are the Z_h and Z_{dr} calculations, based on the
 274 individual scattering amplitudes of drops (i.e., drop-by-drop integration using MoM-SIE or
 275 simply MoM-SIE) over each 1-minute period. The radar measurements of Z_h and Z_{dr} show
 276 good temporal correlation and agreement with the MoM-SIE as well as bulk calculations with
 277 the radar peak values being somewhat larger (60 dBZ and 4 dB) than the simulations perhaps
 278 because of disdrometer sampling limitations for large drops or the applied smoothing. While
 279 the agreement between MoM-SIE and bulk methods for Z_h is expected, the agreement of Z_{dr}
 280 is somewhat unexpected given the large variance in individual drop Z_{dr} values in the line
 281 convection region (see Fig. 4(c)) especially for the large drops. The bulk method Z_{dr} is
 282 essentially related to the reflectivity-weighted mean axis ratio which would equal the drop-
 283 by-drop integrated Z_{dr} if the axis ratio distribution is narrow (Jameson 1983; Bringi and
 284 Chandrasekar 2001). As discussed earlier, the coefficient of variation of the “effective” axis
 285 ratio in the line convection is estimated to be around a factor of 2 larger than the value from
 286 Thurai et al. (2009a) which is based on data from an artificial rain experiment where
 287 *asymmetric* drops were not detected. In spite of this increase, the axis ratio distribution in the
 288 line convection case is judged to be narrow enough that the drop-by-drop MoM-SIE
 289 computed Z_{dr} is in good agreement with the bulk method.

290 Note the radar reflectivity for an individual (i^{th}) drop, in a volume of 1 m^3 , is given by:

$$291 \quad Z_i = 10^{18} \frac{\lambda^4}{\pi^5 |K_w|^2} \eta_i, \quad (3)$$

292 where λ is the wavelength in air, $\eta_{h/v} = 4\pi |S_{hh/vv}|^2$ is back scatter cross section per unit volume
 293 for horizontal/vertical (h/v) polarization, $K_w = (\epsilon_r - 1)(\epsilon_r + 2)^{-1} = 0.9631 - j0.0111$ is the

294 dielectric factor of water at C-band with dielectric constant $\epsilon_r = 72.5 - j22.43$. Over a 1-minute
 295 period, the resulting reflectivity Z is derived by summing the individual drop reflectivities
 296 and is calculated using:

$$297 \quad Z = \frac{1}{A\Delta t} \sum_i v_i^{-1} Z_i, \quad (4)$$

298 where A is the measurement area of the 2DVD, Δt is the averaging time period, and v_i is the
 299 vertical velocity of the i^{th} drop. Equations (3) and (4) are used to evaluate the overall radar
 300 reflectivity based on the individual scattering amplitudes for each of the reconstructed rain
 301 drops as well as their individual measured fall velocities. The computed Z values for h and v
 302 polarizations are converted to the conventional dBZ units and the Z_{dr} in dB is obtained from
 303 the difference between the two.

304 Fig. 6(c) shows the calculated ρ_{hv} values using:

$$305 \quad \rho_{\text{hv}} = \frac{\left| \sum_i v_i^{-1} S_{\text{hh}}^* S_{\text{vv}} \right|}{\sqrt{\sum_i v_i^{-1} |S_{\text{hh}}|^2 \sum_i v_i^{-1} |S_{\text{vv}}|^2}}, \quad (5)$$

306 where v_i is the vertical velocity of the i^{th} drop, S represents single drop back-scattering
 307 amplitude, and the summation is done over all the drops recorded by the 2DVD during the
 308 considered time interval. From 03:35 to 03:40 UTC, a sharp decrease or dip in ρ_{hv} is seen,
 309 reaching as low as 0.8. Such low values are consistent with the radar measurement of ρ_{hv} as
 310 low as 0.85 in the PPI plot in Fig. 5(d). For comparison, C-band scattering calculations using
 311 the 1-minute averaged DSDs and bulk assumptions are included in magenta in Fig. 6(c). The
 312 lowest value using the bulk assumptions is only 0.96. Clearly, the drop-by-drop MoM-SIE
 313 based calculations give rise to much more accurate ρ_{hv} predictions than the bulk method. This
 314 is due to the inability of the bulk method to capture the variability of drop shapes during the

315 line convection passage. Note however, that at other times, i.e., prior to 03:35 UTC and after
 316 03:45 UTC, both methods predict ρ_{hv} values that are close to 1. These values are consistent
 317 with radar measurements over the 2DVD site at these other times. The measurement accuracy
 318 of ρ_{hv} is around 1% which is substantially less than the simulated change from 0.96 to 0.8-
 319 0.85 so the dip should be detectable if the SNR>20 dB or so (Bringi and Chandrasekar 2001).

320 Figure 6(d) compares the specific differential propagation phase (K_{dp}) derived from the
 321 ARMOR range profiles of differential phase (Φ_{dp}) with the corresponding scattering
 322 calculations. For the radar-based K_{dp} values, the finite impulse response (FIR) range filtering
 323 technique is used, as described in Hubbert and Bringi (1995), having the advantage of
 324 quantifying and removing any backscatter differential phase contribution, which at C-band
 325 can become significant when large drops or small melting hail are present in the radar pulse
 326 volume. However, close examination of the phase data showed the backscatter differential
 327 phase $\delta < 3-5^\circ$ along the line convection which discounts the presence of small melting hail
 328 for which δ could reach 20° (Meischner et al. 1991). For the scattering calculations, as in
 329 other panels of Fig. 6, the bulk calculations (assuming rotational symmetry) are shown in
 330 magenta and the MoM-SIE calculations are shown as black line. K_{dp} is calculated from:

$$331 \quad K_{dp} = 10^3 \lambda \frac{180}{\pi} \frac{1}{A\Delta t} \sum_i v_i^{-1} \text{Re}[S_{hh} - S_{vv}], \quad (6)$$

332 where S represents forward scattering amplitudes. The summation is done over all drops
 333 recorded in the considered time interval. The bulk calculations are in good agreement with
 334 the MoM-SIE calculations which indicates that K_{dp} is not dependent on the variance of
 335 shapes, rather it is related to the mass-weighted mean axis ratio (Jameson 1985; Bringi and
 336 Chandrasekar 2001). The radar estimate of K_{dp} is smaller than the calculations due to the
 337 range filtering and smoothing methodology used across the compact line convection region.

338 In Thurai et al. (2017), the cross-polar backscatter from *asymmetric* drops in terms of
339 single-particle (LDR) was also considered. Here we extend to drop-by-drop MoM-SIE LDR
340 calculations as the ratio of the cross-polar reflectivity to the copolar reflectivity and compare
341 that with the bulk method as shown in Fig. 7. It is immediately clear that during the line
342 convection passage, the MoM-SIE method shows much larger LDR than the bulk method
343 (peak of -17 dB versus -26 dB). Even outside the line convection, the MoM-SIE LDR is
344 larger by 3-5 dB relative to the bulk method. We do not have radar data to compare against as
345 the ARMOR radar is not configured for cross-polar reflectivity measurement. However, it is
346 possible to use an analytical equation relating LDR, Z_{dr} , ρ_{hv} , δ and standard deviation of the
347 canting angle (σ_{β}) (Jameson 1987) to illustrate the consistency between the dip in ρ_{hv} and the
348 peak in LDR from MoM-SIE calculations during the line convection passage. Using Eq.
349 (3.232) from Bringi and Chandrasekar (2001) and setting the values of $Z_{dr}=3$ dB, $\rho_{hv}=0.8$,
350 $\delta=5^\circ$ and $\sigma_{\beta}=10^\circ$ predicts LDR of -19 dB which is consistent with MoM-SIE peak LDR of -17
351 dB coinciding with dip in ρ_{hv} to 0.82 (close to radar measured dip of 0.8). On the other hand
352 under the same conditions, setting LDR in Eq. (3.232) to the bulk peak value of -26 dB
353 predicts a much larger $\rho_{hv}=0.97$ (the dip in bulk ρ_{hv} is only to 0.96). Thus, assuming that the
354 radar measured dip in ρ_{hv} to 0.8 is accurate, we can infer that the MoM-SIE calculated LDR
355 peak of -17 dB is more consistent with radar dip in ρ_{hv} than the bulk peak of -25 dB. It
356 follows that the large MoM-SIE LDR values in the line convection are due to enhanced
357 variance in drop shapes due to presence of *asymmetric* drops which cannot be modelled using
358 the bulk method. Over the entire 100-minute event, Table 1 shows the relative frequency of
359 occurrence of MoM-SIE and bulk LDR values in 5 dB bins. The modal value (at bin center)
360 of LDR for MoM-SIE and bulk method are, respectively, -37.5 and -32.5 dB with the MoM-
361 SIE showing positive skewness.

362 It should also be noted that because the scattering amplitudes for *asymmetric* drops
363 exhibit ϕ dependence, as we saw earlier in Fig. 3, it is necessary to choose the correct ϕ angle,
364 particularly for the Z_{dr} calculations. In our case, the azimuth angle from the radar to the
365 2DVD site was 52 degrees, and our reconstruction of drops is referenced to the true North
366 (since the 2DVD was aligned in such a way that this criterion was met), hence we chose the
367 same value for ϕ . In Fig. 8, we compare the single particle Z_{dr} for $\phi = 50, 110, \text{ and } 180$
368 degrees. Also shown is the [1:1] line. As seen the correlation is high with negligible bias in
369 both plots and as a result any significant ϕ dependence would not be expected when the
370 overall Z_{dr} is calculated for all drops over a 1-minute integration period.

371 A limitation of the drop reconstruction procedure is that for a given $z = \text{constant}$ plane,
372 there are only four points available from the two orthogonal cameras, and the 4-ellipse
373 quarters constructed in this plane can have uncertainties in-between these four points.
374 However, because rain drops do not have sharp discontinuities (unlike snow particles), and
375 further they are homogeneous, the resulting errors in the corresponding scattering
376 calculations are not likely to be significant. Another limitation is that deskewing *asymmetric*
377 drop shapes relies on the accuracy of estimating the horizontal drop speed and direction. In
378 the future we will evaluate if the wind speed and direction measured at the height of the
379 2DVD sensor area can be used to deskew asymmetric drops.

380 Another possible source of errors when comparing disdrometer-based estimates against
381 radar measurements is the different spatial scales of the radar and ‘point’ 2DVD
382 measurements as well as the height of the radar pulse volume above the surface (340 m in our
383 case). At short ranges considered herein (15 km) the temporal decorrelation between radar
384 and 2DVD is likely to be constrained as evident in Fig. 6. It is well-known that surface point
385 measurements cannot be representative of the radar pixel which is often quantified in terms of

386 point-to-area variance (Ciach and Krajewski 1999; Thurai et al. 2012) which depends on the
387 spatial correlation function of the observable used in the comparison. Other sources of errors
388 include radar-measurement errors and disdrometer-sampling errors. However, it is beyond the
389 scope of this paper to quantify the error variances arising from such error sources (we refer to
390 Thurai et al. 2012 for variance analysis using ARMOR and 2DVD data).

391

392 **6. Discussion and Conclusions**

393 The bulk method of simulating radar observables such as $[Z_h, Z_{dr}, K_{dp}, \rho_{hv}, LDR]$ in rain
394 involves simplifying assumptions, the main one being related to neglecting the effect of
395 variance in shapes due to presence of *asymmetric drops*, if in fact they occur in significant
396 proportion to the more ubiquitous equilibrium (axisymmetric) shapes. There are very few
397 computations of radar observables that explicitly account for variance in drop shapes. Keat et
398 al. (2016) used the data from an artificial rain experiment reported in Thurai and Bringi
399 (2005) to simulate steady state axisymmetric drop oscillations (assuming Gaussian axis ratio
400 *pdf*) and its effects on ρ_{hv} and Z_{dr} using gamma distribution of drop sizes (DSD) and
401 Rayleigh-Gans theory. Their goal was to retrieve the shape parameter μ of the gamma DSD
402 from radar measurements of $[\rho_{hv}; Z_{dr}]$. Their bulk simulations indicated drop oscillations had
403 to be taken into account in order for the radar-based retrieval of μ to be unbiased. Thurai et al
404 (2009b) used 2DVD measurements to simulate drop-by-drop scattering but assumed
405 symmetric shapes and canting angles derived from the deskewing procedure as in Huang et
406 al. (2008). The agreement with ARMOR radar measurements was good but they found
407 significant differences in Z_{dr} and ρ_{hv} when compared with bulk methods in one convective
408 rain event.

409 To the best of our knowledge this study is the first polarimetric scattering analysis of a
410 line convection rain event based on drop-by-drop scattering computations by means of a
411 higher order method of moments in a surface integral equation formulation, with *asymmetric*
412 drop geometries being reconstructed from 2DVD measurements. We have compared MoM-
413 SIE surface model discretization results for an example asymmetric drop with equi-volume
414 drop diameter $D_{eq}=4.81$ mm (in Fig. 1) at S, C, and X bands with volumetric discretization
415 results by an industry standard finite element method based code (HFSS), showing excellent
416 agreement between two methods. The single particle Z_{dr} values showed variability during the
417 passage of the line convection over the 2DVD site with coefficient of variation (when Z_{dr} is
418 expressed as a ratio) of around 0.5 (for drops > 3 mm) which confirms that the variance of
419 drop shapes due to asymmetric drops can be an important factor in this particular case. Note
420 that before and after passage of the line convection the shape variability was sharply reduced.

421 Drop-by-drop scattering calculations based on 1-minute integration of the covariance
422 matrix elements were performed for the 100-minute event passage over the 2DVD site using
423 the MoM-SIE and the bulk methods. The simulated radar observables were compared with
424 ARMOR radar data extracted from range gates surrounding the 2DVD location. The Z_h , Z_{dr}
425 and K_{dp} were found to be in good agreement between the MoM-SIE, the bulk calculations and
426 the extracted ARMOR data during the line convection passage as well as before and after the
427 passage. However, the bulk method could not simulate the significant lowering of ρ_{hv} during
428 the line convection with dip to 0.8 as measured by radar. The MoM-SIE calculations were
429 able to simulate the dip to 0.8 indicating that the lowered values were a result of variance in
430 shapes due to asymmetric drops. The radar differential phase data showed no evidence of
431 backscatter differential phase (estimated $\delta < 3-5^\circ$) within the line convection and neither did

432 the single drop MoM-SIE calculations ($\delta < 5^\circ$), so this effect could not have contributed to
433 the lowering of ρ_{hv} .

434 We also computed LDR using drop-by-drop MoM-SIE and the bulk method. During the
435 line convection passage over the 2DVD the MoM-SIE LDR values peaked to -17 dB whereas
436 the bulk LDR was around 8 dB lower (-25 dB). Examination of an analytic expression
437 relating the polarimetric variables showed that the MoM-SIE LDR peak of -17 dB was
438 consistent with the dip in ρ_{hv} to 0.8 (the latter in agreement with the radar observed dip).
439 However, the bulk LDR of -25 dB was not consistent with the observed ρ_{hv} dip, the analytic
440 expression giving a much higher ρ_{hv} value of 0.97 consistent with the calculated bulk value of
441 0.96. Since the ARMOR radar was not configured for LDR measurements we could not
442 compare with the simulated values. Over the full 100-minute event the modal MoM-SIE LDR
443 values were around -32.5 dB whereas it was around -37.5 dB for the bulk method. Radars
444 with modest dual-polarized antenna with a system LDR limit of -25 dB (e.g., phased-array
445 airborne radars) could easily detect the LDR peak of -17 dB. However, to detect LDR of -
446 32.5 dB a well-designed antenna capable of system LDR limit of -36 dB would be required
447 (the UK C-band operational radars approach the -36 dB system limit and they routinely
448 measure LDR to detect wet snow aloft; Sandford et al. 2017).

449 As has been mentioned in earlier publications (Thurai et al., 2013; 2014), 2DVD data
450 examined during most of the rain events showed that the drop shapes conform to the ‘most
451 probable’ shapes arising from the steady state axisymmetric oscillation mode which can be
452 regarded as the background state. *Asymmetric* shapes occur when the background state is
453 perturbed due to transverse or horizontal modes mixed in which is termed as mixed-mode
454 oscillations (Beard et al. 2010). The line convection system considered here is one of the few
455 exceptions where a significant proportion ($\approx 30\%$) of *asymmetric* drops was only detected

456 within the line convection but not outside it. Currently, there is no theoretical framework to
457 identify the conditions under which mixed mode oscillations may occur in a persistent
458 manner. For now we have to rely on 2DVD data to first detect the presence of a significant
459 proportion of asymmetric drops in the rain shaft and subsequently to evaluate the conditions
460 under which deviations from the ‘most probable’ axisymmetric drop shapes occur. Based on
461 this study the most impact would be on quantitative use of ρ_{hv} and LDR with much less
462 impact on Z_{dr} and negligible impact on Z_h and K_{dp} .

463

464

465

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468 observations used in this NSF study.

469

470 The 2DVD data (in the form hyd/hd files) used in this study can be made available upon
471 request from Dr. M. Thurai (email: merhala@colostate.edu), or Dr. P. N Gatlin (email:
472 patrick.gatlin@nasa.gov) or Dr. M. Schönhuber (email: michael.schoenhuber@joanneum.at).
473 ARMOR radar data are archived at University of Alabama @ Huntsville, and can be also
474 made available.

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659 Figure 5: PPI scans of (a) attenuation-corrected Z_h , (b) attenuation-corrected Z_{dr} , and (c) ρ_{hv} ,
660 taken at (top to bottom) 03:40 UTC when the line convection was directly above the 2DVD
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662 areas within the line convection where ρ_{hv} values were lower than 0.9. :

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664 Figure 6: Polarimetric radar variables comparison between MoM-SIE, bulk method, and
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666 correlation coefficient (ρ_{hv}), and (d) Specific differential propagation phase (K_{dp}). The grey
667 line in Fig. 6(d) represents the same MoM-SIE based calculations but with averaging done
668 over a 1-minute time interval rather than 5-minute period.

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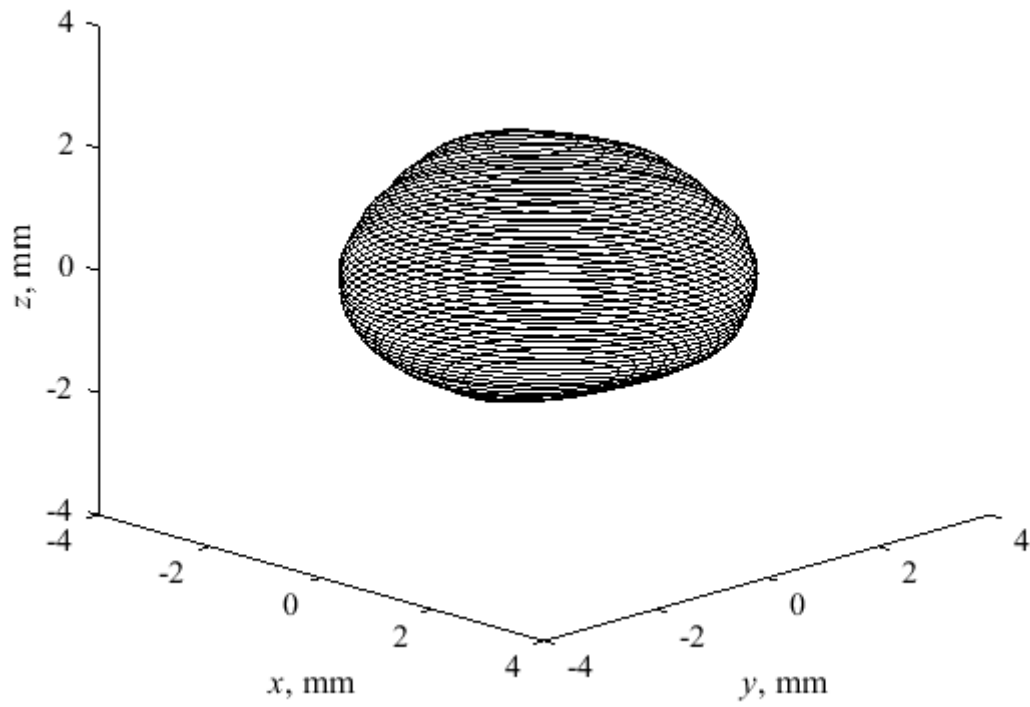
670 Figure 7: LDR computation for incident $\phi=50^\circ$ and 1 minute averaging.

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672 Figure 8: Single particle Z_{dr} comparison for particles with $D_{eq} \geq 2$ mm for $\phi = 50$ degrees
673 versus $\phi = 180$ degrees (left) and for $\phi = 50$ degrees versus $\phi = 110$ degrees (right). The
674 purple dashed line represents the [1:1] line.

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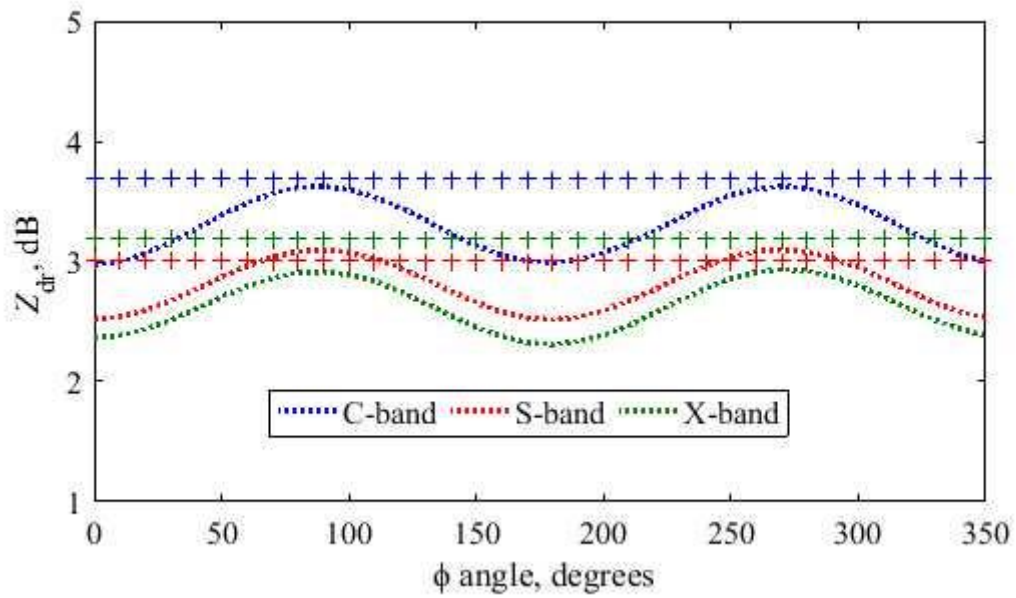


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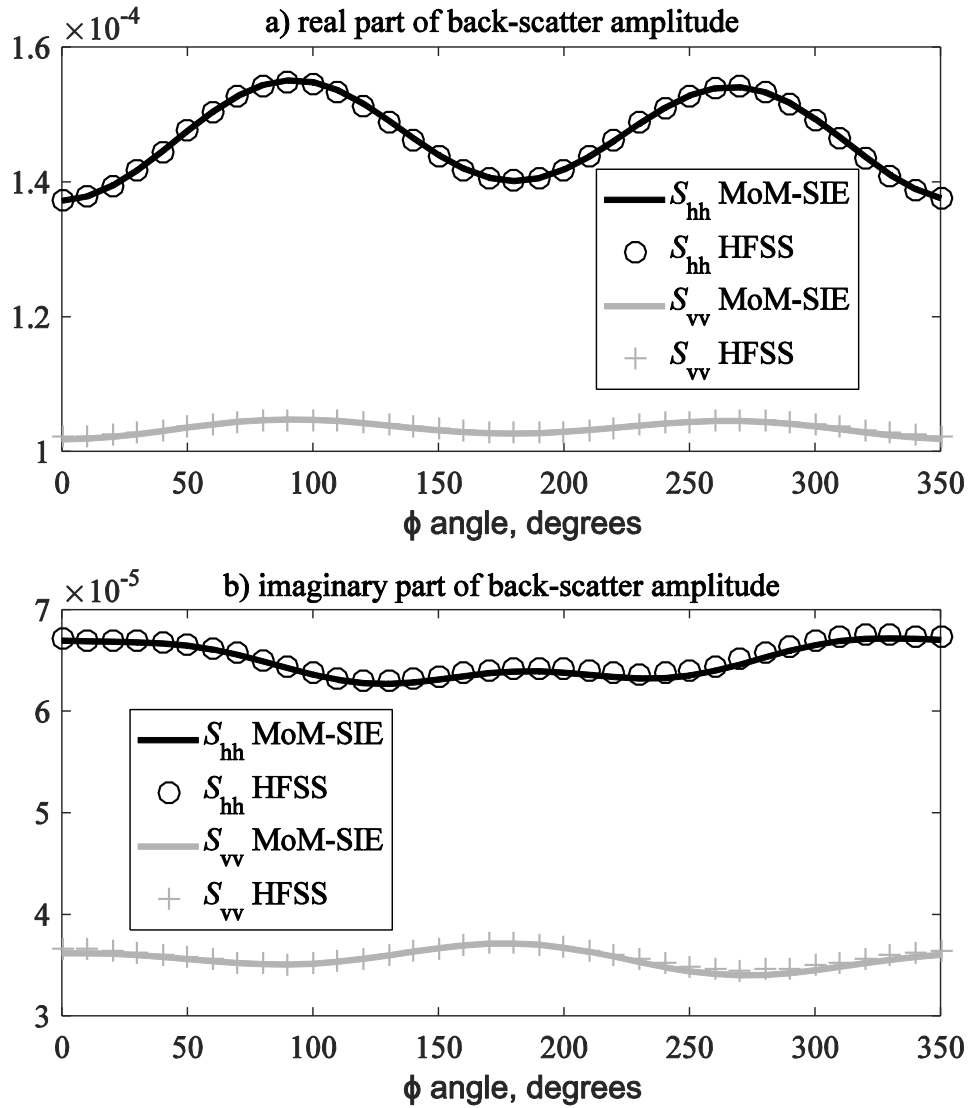
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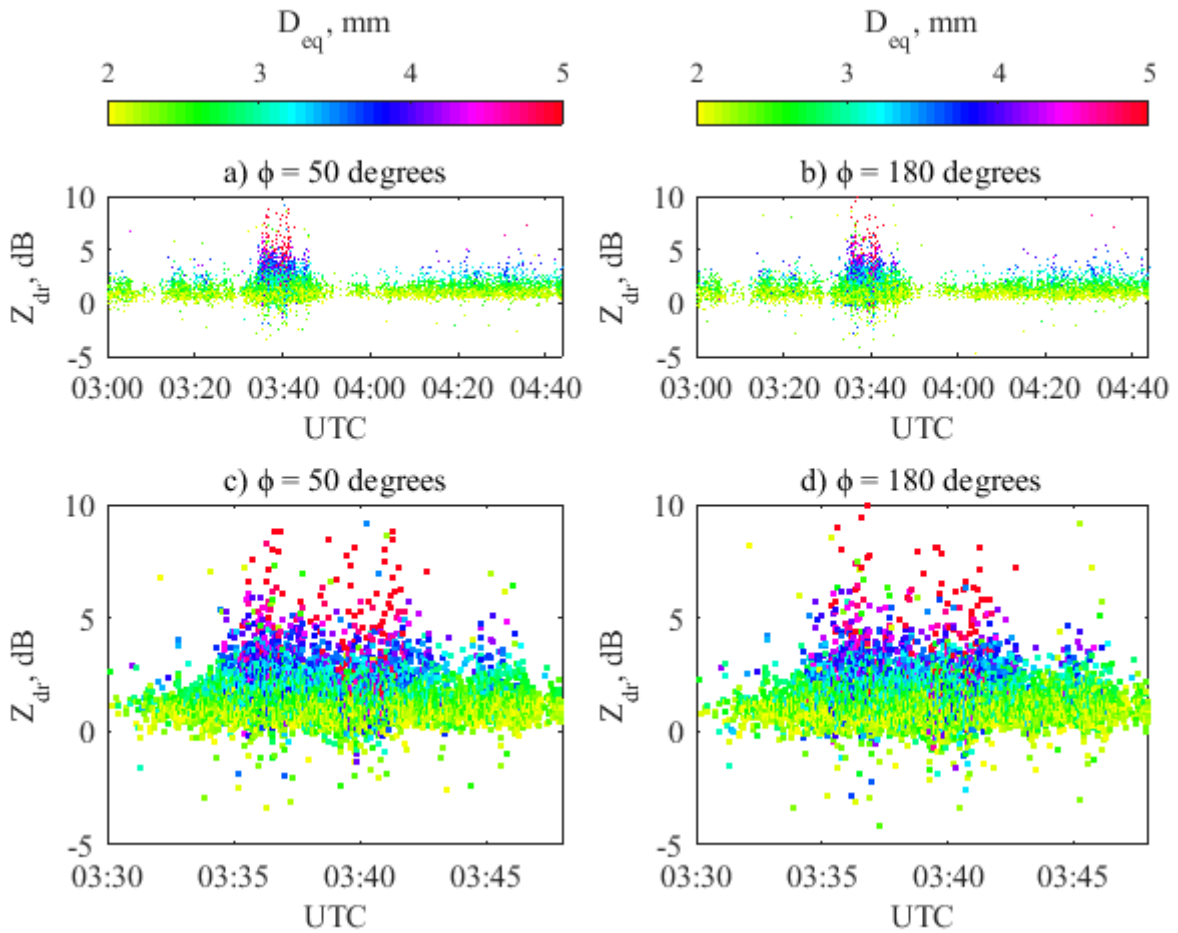
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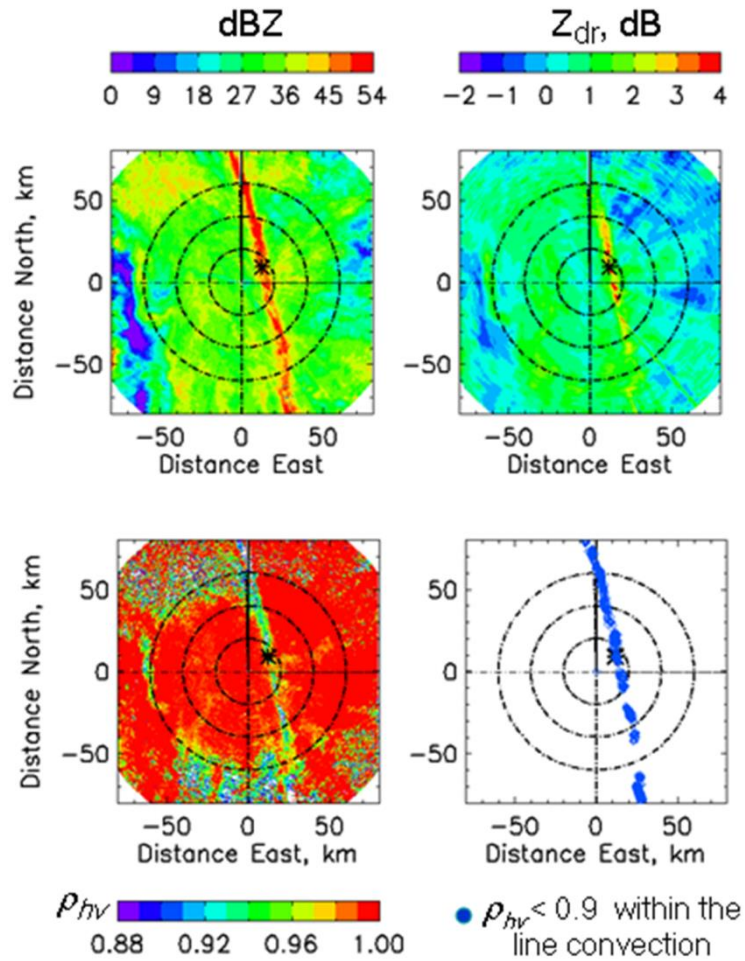
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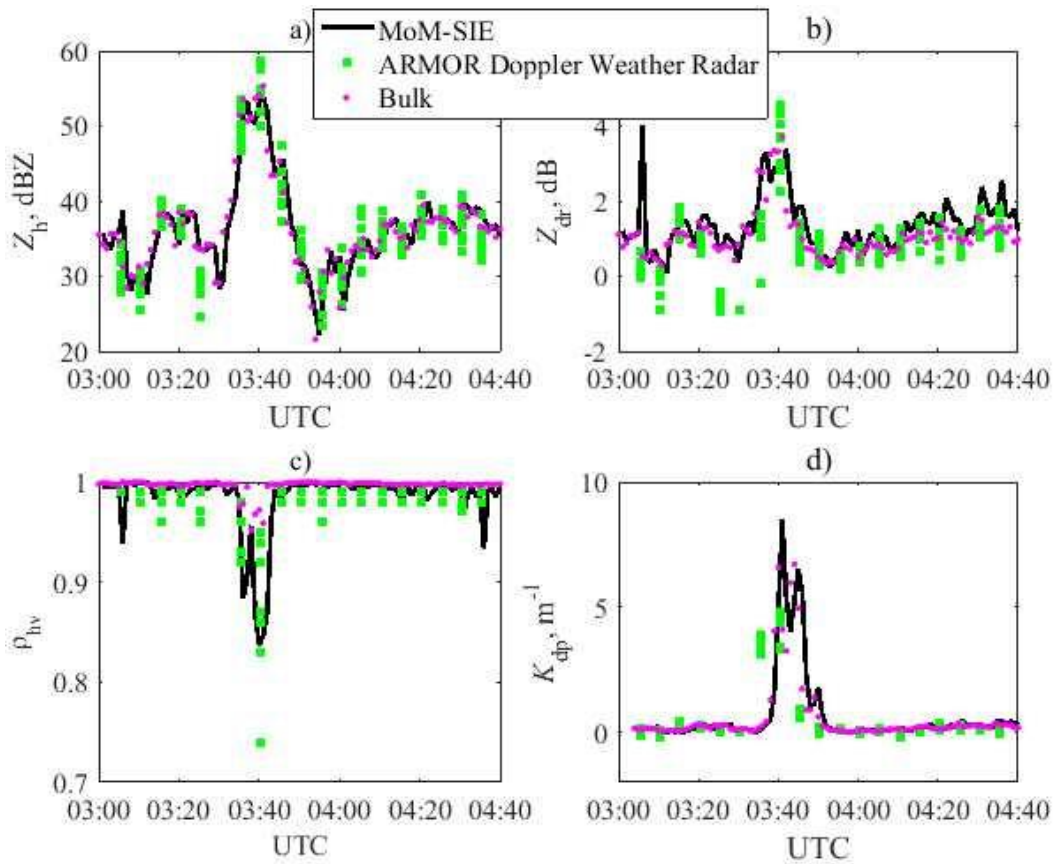
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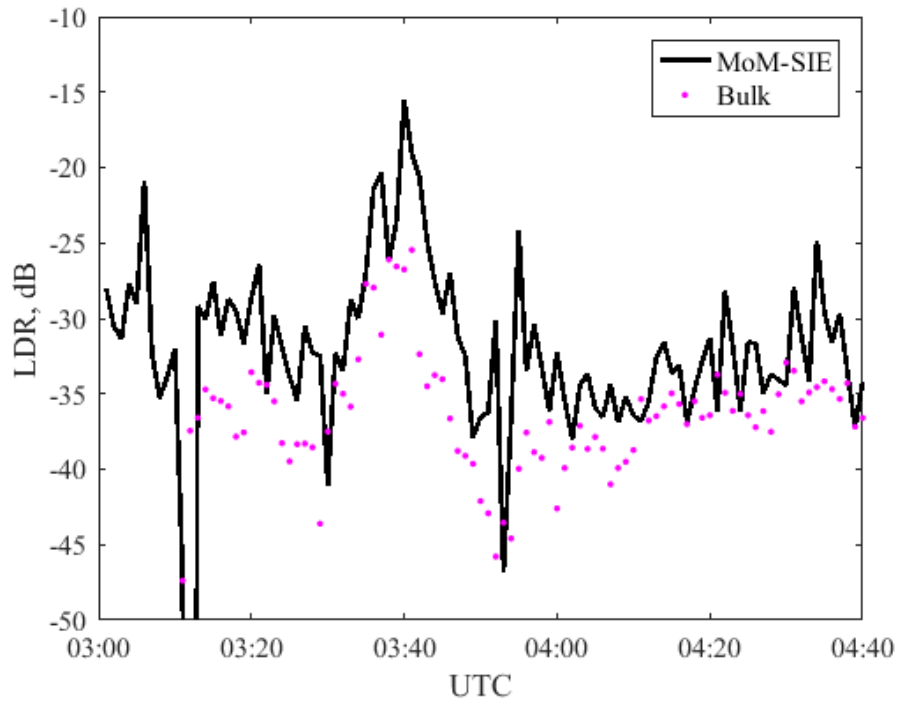
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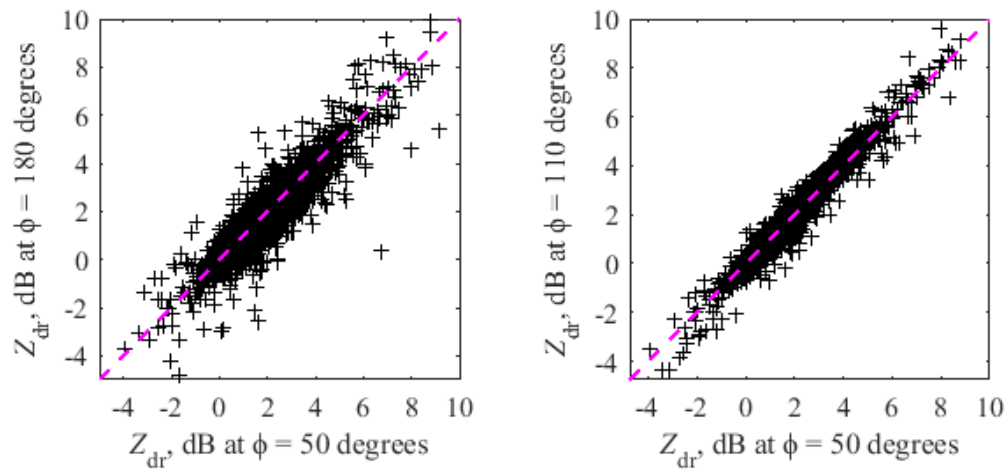


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716 purple dashed line represents the [1:1] line.

717

718

Table 1

719

Relative frequency of occurrence (in %) of MoM-SIE and bulk LDR values in 5 dB bins

720

computed with drop-by-drop MoM-SIE and bulk T-matrix methods

721

Range of LDR, dB	T-matrix	MoM-SIE
< -40	21.3	3.96
-40 to -35	49.2	19.8
-35 to -30	19.7	46.54
-30 to -25	9.8	19.8
-25 to -20	0.0	7.92
-20 to -15	0.0	1.98
-15 to -10	0.0	0
> -10	0.0	0

722